

# LUEHR FILTER

## **Conditioned chemisorption as an easy and well-proven method of gas cleaning downstream waste and RDF-incinerators**

**Ruediger Margraf**

LUEHR FILTER GmbH & Co. KG, 31655 Stadthagen, GERMANY



**ISWA Conference, Moskau**

31 May – 2 June 2011

## Contents

	Abstract.....	3
1	Introduction.....	4
2	Conditioned dry sorption by means of Conditioning Rotor – Recycle Process	
2.1	General description .....	6
2.2	Conditioning rotor .....	8
2.3	Application examples .....	9
3	Conditioning Rotor – Recycle Process with graded additive powder injection .....	13
3.1	Application example .....	14
4	Utilisation of CaO instead Ca(OH) <sub>2</sub> for reduction of operating costs .....	16
5	Advantages of conditioned dry sorption compared of the spray sorption .....	18
6	Assessment .....	19

**Abstract**

Following to the tightening of emission limit values in Europe between 1980 and 1990, complex, multi-stage plants have been installed for the gas cleaning downstream waste incinerators. As a result of the extremely high investment and operating costs, the waste incineration was no longer economical. Due to the consistent advancement of semi-dry procedures, high-efficient cleaning systems could be developed, with reliable observance of the requested emission limit values at considerably lower investment and operating costs.

The Chemisorption with particle conditioning offers such a procedure. It mainly comprises the component parts additive powder injection ( $\text{CaO}/\text{Ca(OH)}_2$ , AC), reaction chamber, fabric filter and multiple particle re-circulation with wetting of recycled particulate prior to reinjection into reactor. This system allows the simultaneous separation of particles, heavy metals, incl. mercury and mercury compounds, acid crude gas components such as HF, HCl,  $\text{SO}_x$  as well as dioxins / furans. Especially the approx. 50fold particle re-circulation combined with the wetting of the recycled particulate grants the high effectiveness of this system with regard to the separation capacity and the additive powder consumption.

The efficiency is described on the basis of several application examples out of the field of waste incinerators. The presentation includes among other things the degrees of separation and the emission limit values in comparison with definitely more complex scrubbing systems.

The process is in addition provided with an up-to-date control device for the additive powder injection. Based on crude gas measurements of the acid crude gas components HCl and  $\text{SO}_x$  as well as on measurements of the volume flow, the additive powder is injected in dosed quantities in accordance with a given stoichiometric factor. The control concept is explained by means of a practical example.

Furthermore, results will be presented, showing the advantages of the Chemisorption with particle conditioning relating to the expenses for consumable supplies, compared to a conventional spray sorption for the separation of acid crude gas components.

## 1 Introduction

In the space of time between 1980 and 2000, the emission limit values for Waste-to-Energy-plants have considerably been tightened in several steps in Germany and Europe. The currently valid limit values are fixed in the

- EU Directive 2000/76/EG of the European Parliament and the board of the incineration of waste, dated 04.12.2000
- 17 BImSchV. – Regulation for the application of the federal emission protection law (regulation concerning the incineration and co-incineration of waste) – valid for Germany since 23.11.1990.

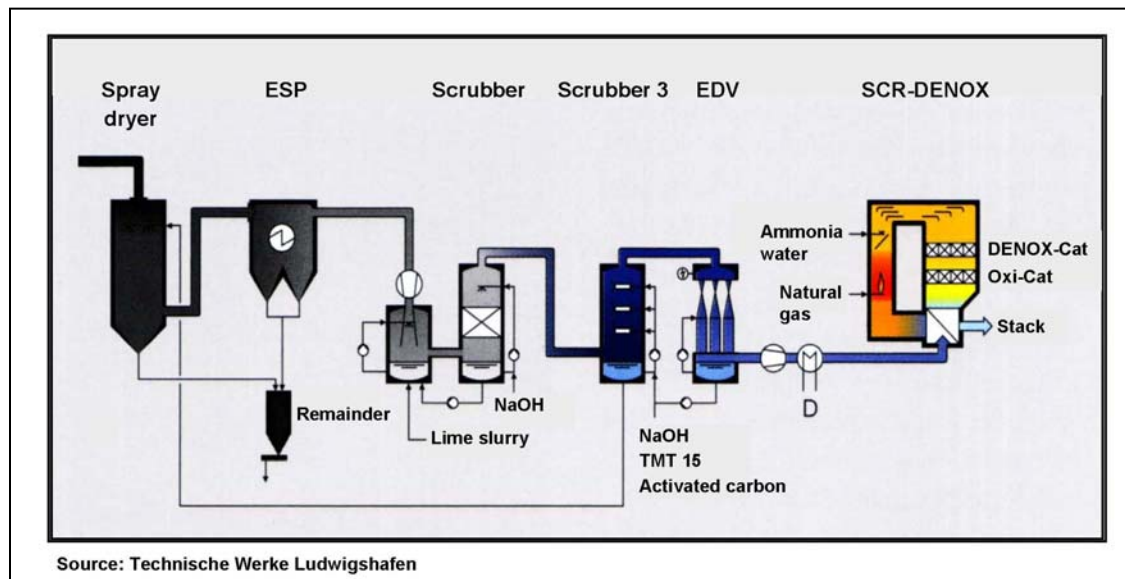
Table 1 shows the relevant limit values of the EU directive to be observed regarding the design of flue gas treatment plants downstream waste incinerators.

		DAV	HAV
Overall dust	mg/m <sup>3</sup> / gr/scf	10 / 0.004	30 / 0.012
Overall carbon *	mg/m <sup>3</sup> / ppm	10 / 18	20 / 36
HCl	mg/m <sup>3</sup> / ppm	10 / 6	60 / 36
HF	mg/m <sup>3</sup> / ppm	1 / 1	4 / 4
SO <sub>2</sub>	mg/m <sup>3</sup> / ppm	50 / 17	200 / 70
NO <sub>x</sub> *	mg/m <sup>3</sup> / ppm	200 / 97	400 / 194
CO *	mg/m <sup>3</sup> / ppm	50 / 40	100 / 80
		Average over sampling period	
Cd + Tl	mg/m <sup>3</sup>	0.05	
Hg + Hg compounds	µg/m <sup>3</sup>	30	50
Σ Heavy metal	mg/m <sup>3</sup>	0.5	
Dioxin + Furan	ng/m <sup>3</sup>	0.1	
* Reduction measures within boiler			
DAV = Daily average value / HAV = Half-hour average value			

Tab. 1: Summary of relevant emission limit values accord. to EU Directive 2000/76/EG

Furthermore, in 2006, the countries of the European Union passed the “reference document on the best available techniques for waste incineration“. This guideline describes the different, available gas cleaning systems. Chapter 5 of this lecture specifies the best available techniques (BAT) with the corresponding advantages and disadvantages. Technologies, which are not listed, cannot be used for the gas treatment at waste incineration plants.

As a result of the tightened limit values, new plants were provided with complex, multi-stage flue gas cleaning systems for the waste combustion. With regard to existing plants, several additional separation stages had to be upgraded for separate gas substances in order to observe the emission limit values. An example for this is the WtE plant Ludwigshafen/Germany (ill. 1).



III. 1: Schematic view of gas cleaning system installed at WtE plant Ludwigshafen in 1994

After upgrading in the course of the years until 1994, the flue gas cleaning system installed at this plant comprises 6 stages.

The installation of such complex gas cleaning systems involved high investment and operating costs, thus limiting in the end the economical efficiency of waste incinerators. In order to improve the competitiveness compared to others disposal systems, it became necessary to find simpler technologies for the reliable observance of the requested emission limit values. As a result of the consistent development of dry and semi-dry separation technologies, simple procedures are nowadays available as alternative.

- Chemisorption with particle and gas conditioning Additive powder:  $\text{Ca}(\text{OH})_2$  and activated coke/ activated carbon (AC)
- Dry sorption  
Additive powder:  $\text{NaHCO}_3$  and activated coke/activated carbon (AC)

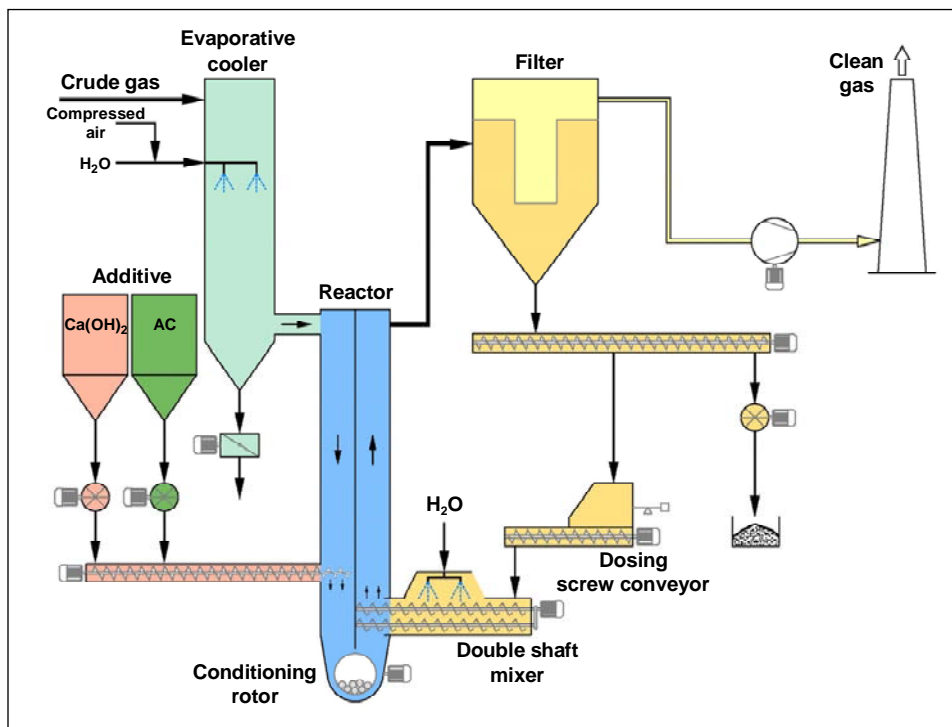
Following to chapter 5 of BREEF notes, both technologies are defined as the best available technology.

Whereas the dry sorption with  $\text{NaHCO}_3$  has only been realised on a comparatively small scale due to the high purchase costs for the  $\text{NaHCO}_3$ , the semi-dry absorption with utilisation of Ca-based additive powders became widely accepted. Considering the approx. 30 new plants for the incineration of waste or RDF (Refuse Derived Fuel) realised in Germany in the years 2005 up to the end of 2009, a large part of them has been provided with this process technology. The Conditioning Rotor – Recycle Process with particle conditioning is one type of execution of this sorption technology. It allows the simultaneous separation of particles, heavy metals incl. mercury and mercury compounds, acid crude gas components such as HF, HCl and  $\text{SO}_x$  as well as dioxins/ furans.

## 2 Conditioned dry sorption by means of Conditioning Rotor – Recycle Process

### 2.1 General description

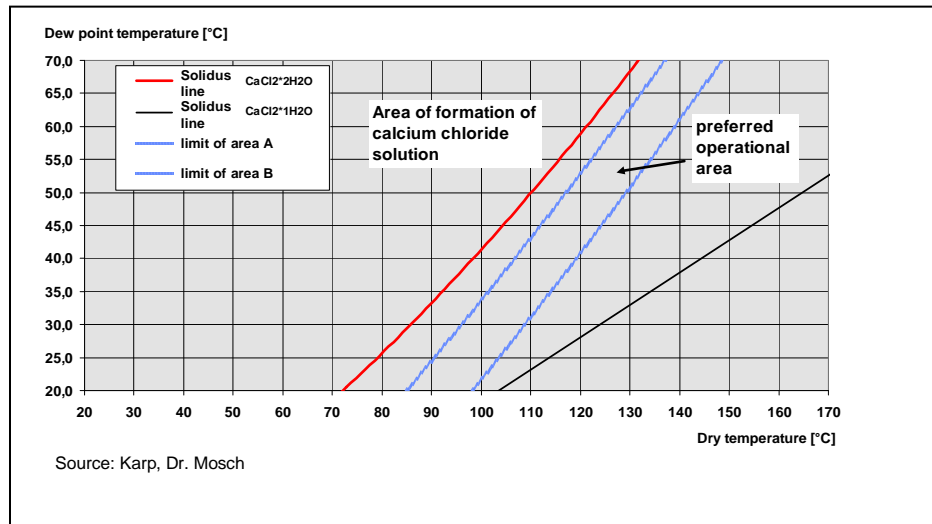
A schematic view of the Conditioning Rotor – Recycle Process with particle conditioning is given in illustration 2. It mainly comprises the component parts evaporative cooler, additive powder injection, conditioning rotor reactor, fabric filter as well as particle re-circulation with integrated particle conditioning.



Ill. 2: Schematic view of Conditioning Rotor – Recycle Process with particle and gas conditioning

The evaporative cooler (gas conditioning) serves for the optimum temperature adjustment for the reaction between the additive particles and the acid gas molecule, combined with an increase in the absolute and relative humidity for the optimisation of the separation efficiency with at the same time good additive powder utilisation.

Whereas in case of use of Ca-based additive powders, the separation of  $\text{SO}_3$  and HF takes place with a high reaction velocity in the complete temperature range, the dry temperature as well as the absolute and relative humidity in the gas have a considerable influence on the HCl and  $\text{SO}_2$  separation. Decreasing temperature and increasing humidity will improve the efficiency. Depending on the parameters of an application, the min. admissible operating temperature has to be chosen in that way, that deposits and blockages, especially due to the hygroscopic features of  $\text{CaCl}_2$  particles, will be avoided within the plant. The preferred operating range for the dry temperature depending on the dew point temperature is shown in illustration 3.



III. 3: Phase diagram  $\text{CaCl}_2 \times n \text{H}_2\text{O}$

The separation stage, composed of conditioning rotor reactor with additive powder injection, fabric filter and multiple particle re-circulation incl. particle conditioning, serves for the following:

- Creation of good reaction conditions of up to  $n \times 100 \text{ g/m}^3$  due to the particle re-circulation. Especially when realising high, up to 50fold, additive powder recycle rates, the particle recirculation demonstrably leads to a considerable improvement of the separation capacity regarding acid crude gas components and/or to a reduction in the additive powder injection rate.
  - Increase in residence time of additive powder particles in the system.
  - Higher additive powder density near the reactor upstream filter (the reaction time within reactor amounts to up to  $> 2 \text{ sec.}$ ).
  - A frequent, spatial new orientation of the re-circulated additive powder particles with rebuild of filter cake on the filter fabric.

It should be noted that the multiple particle recirculation also has an advantageous effect on the reliable observance of limit values for dioxins/ furans and mercury as well as mercury compounds with an at the same time low injection quantity of AC. The large additive powder potential within the system also helps to observe reliably the limit values during Hg peaks.

Improvement particularly with regard to the  $\text{SO}_2$  separation, due to the wetting of the re-circulated particulate. As described before and as a result of the increase in the absolute and relative humidity of the flue gas, the gas conditioning has a positive effect on the sorption output. However, a good additive powder efficiency, especially for the separation of  $\text{SO}_2$ , can only be achieved if the water steam partial pressure lose to the additive particles lies at least for a short time in the range of the saturation steam pressure. This will be achieved by wetting of the recycled particulate prior to reinjection into the reactor. Up to the evaporation of the water injected into the humidifying mixer, the wetting causes an increase in the water steam content at the

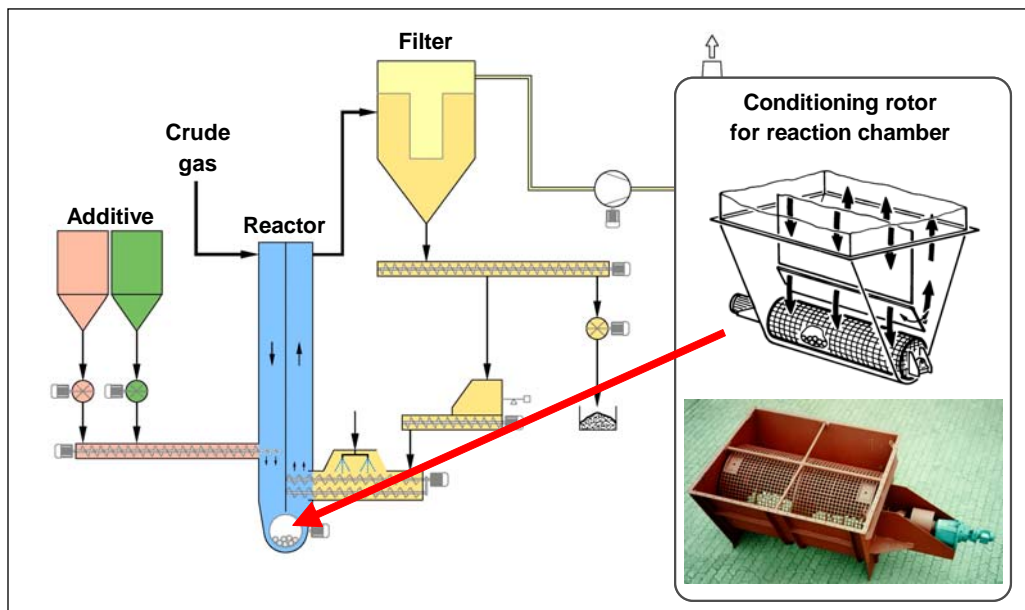
surface of additive powder particles, thus improving the reactivity regarding the acid crude gas components.

In most of the cases, due to the limited proportional wetting of recycled particulate, the installation of an evaporative cooler upstream reactor will be necessary to adjust the optimum reaction temperature.

## 2.2 Conditioning rotor

Due to the requested, necessary high particle recycle rates and in order to grant an optimum additive powder efficiency, it will be necessary to use re-circulation systems which can reliably handle considerable recycling quantities, even if larger quantities of difficult particles, such as  $\text{CaCl}_2$ , are present in the particle spectrum. The Conditioning Rotor – Recycle Process offers a technology which has been applied successfully for many years for various fields of application. The transport of particles from the filter to the reactor takes place mechanically. Conveying with pneumatic methods, which is prone to frequent breakdowns, is not used.

The conditioning rotor is located in the lower reaction chamber elbow of the two-pass reactor (ill. 4). The rotor is a hollow cylinder, made of a perforated plate with openings of approx. 1 x 1 inch. Up to 10% of its volume is filled with balls made of heat-and wear-resistant ceramics. The rotor is supported on both sides, outside of the adjacent walls, and is continuously rotating with approx. 1 rpm by means of a geared motor. The rotation causes the balls to move relatively to each other inside of cylinder and to the perforated shell.



Ill. 4: Conditioning rotor


The objectives of a conditioning rotor are:

- Avoidance of particle deposits when reversing a particle-laden gas flow
- Achievement of a homogeneous distribution of new additive powder injected into the gas flow in reactor
- Disintegration of larger agglomerates with a descent velocity higher than the transport velocity in the ascending part of reactor

The wetted re-circulated particles cannot be injected in the gas flow upstream conditioning rotor but descending agglomerates will be disintegrated to such an extent that they can be carried along with the gas flow towards the filter. A discharge system underneath the reaction chamber elbow will not be necessary.

## 2.3 Application examples

Representing many realised plants with Conditioning Rotor - Recycle Process and particle conditioning, illustration 5 shows the gas cleaning system of line no. 2 of the WtE plant in the city of Ludwigshafen/Germany. Furthermore, in addition to the photo of plant, a table shows the crude gas values downstream boiler. The emission limit values to be observed correspond, for most of the gas substances, to the requirements of the EU directive. Furthermore, regarding SO<sub>2</sub>, a limit value of 9 ppm and for Hg a limit value of 15 µg/Nm<sup>3</sup> has to be observed.

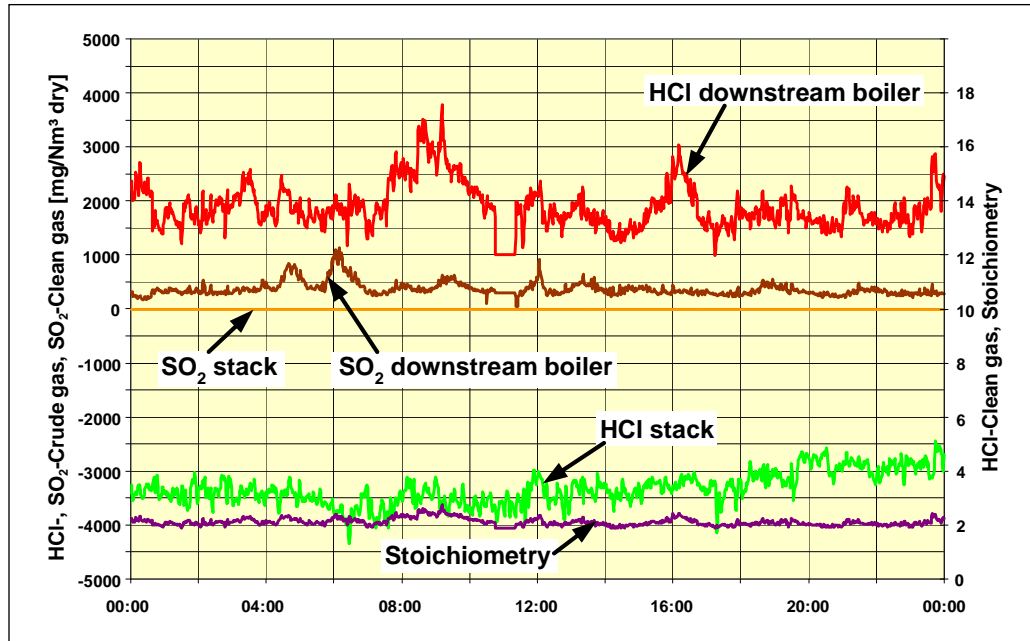


		Gas take-over		Emission limit values	
		DAV	HAV	DAV	HAV
Overall dust	[gr/scf]	0.64	2	0.004	0.008
HCl	[ppm]	620	1,240	6	36
HF	[ppm]	17	34	1	4
SO <sub>2</sub>	[ppm]	150	225	9	45
Hg	[µg/Nm <sup>3</sup> dry]	300	300	15	30
Cd + Tl	[mg/Nm <sup>3</sup> dry]	1.0	3.0	0.05 *	
Σ Heavy metal	[mg/Nm <sup>3</sup> dry]	20	50	0.5 *	
Dioxin / Furan	[ngTE/Nm <sup>3</sup> dry]	3.0	5.0	0.1 *	

\* Average value over sample taking period

III. 5: WtE plant Ludwigshafen/ Germany

Illustration 6 shows the trend curves of crude gas and clean gas values for HCl and SO<sub>2</sub> over a period of 24 hours as well as the stoichiometric factor for the Ca(OH)<sub>2</sub> injection.



III. 6: Trend curves crude gas/ clean gas values and stoichiometry

In case of an average HCl crude gas value of approx. 2,000 mg/Nm<sup>3</sup>, clean gas values of approx. 5 mg/Nm<sup>3</sup> will be achieved. The SO<sub>2</sub> crude gas values of in average approx. 450 mg/Nm<sup>3</sup> will be separated to approx. 100%. The stoichiometry totals to a factor of approx. 2.

Table 2 shows the results of a dioxin measurement. The specific injection quantity of AC totals to approx. 0.03 gr/scf. Even the requested emission limit values for Hg will reliably be kept in continuous operation with this injection quantity.

**Summary of measuring results**

The table below shows a summary of measuring results.

The concentrations are referred to the standard conditions (1.013 hPa, 273 K) and dry exhaust gas.

Measurement	1	2	3
Dust [mg/m <sup>3</sup> ]	1.4	< 1.0	< 1.3
PCDD/PCDF [ng/m <sup>3</sup> ]	< 0.001	< 0.001	< 0.001
I-Teq. accord. to annex 17 BImSchV			

In the following table the concentrations are referred to standard conditions (1.013 hPa, 273 K), dry exhaust gas and addition to an oxygen content of 11 %Vol.

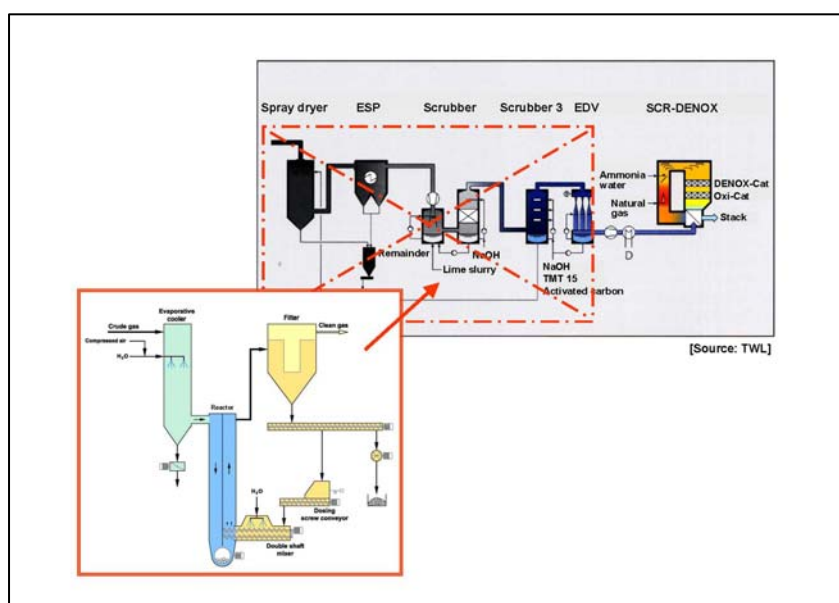
Measurement	1	2	3
Dust [mg/m <sup>3</sup> ]	1.1	< 0.9	< 1.1
PCDD/PCDF [ng/m <sup>3</sup> ]	< 0.001	< 0.001	< 0.001
I-Teq. accord. to annex 17 BImSchV			

Source: ANECO / 04 8077/3 E

Tab. 2: Results of dioxin/furan measurement WtE plant Ludwigshafen

The supervision of the emission limit value for Hg as well as for HCl, SO<sub>2</sub> and dust, takes place by means of continuous measuring instruments in the stack.

The conditioned dry gas cleaning system installed in 2004, replaced a definitely more complex, wet system, consisting of spray dryer, ESP, multi-stage scrubber and aerosol separator (illustration 7).

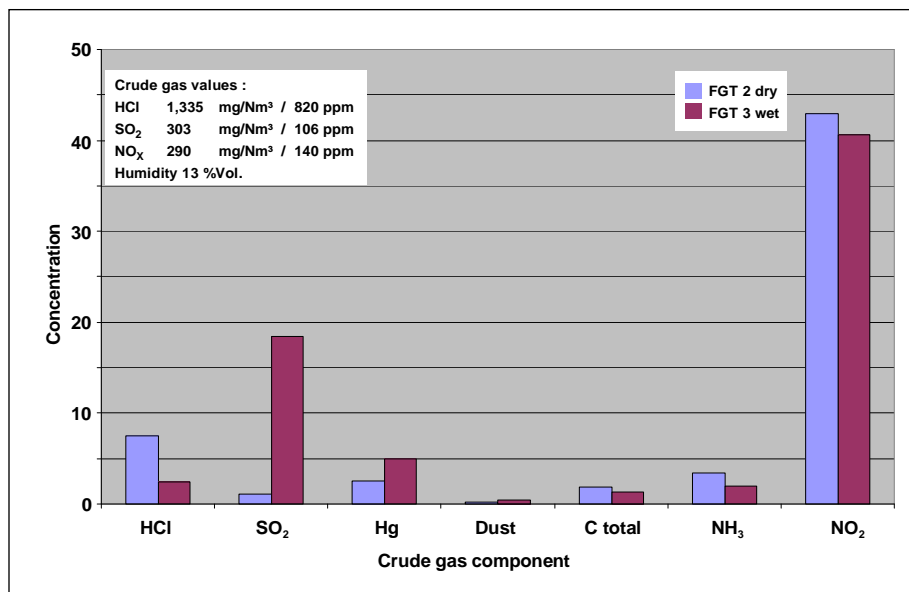


### III. 7: Upgrading of WtE plant Ludwigshafen from „wet“ to „conditioned dry“

Up to the year 2008, another wet flue gas treatment system had been operated in parallel at the waste incinerator in Ludwigshafen until its upgrading, thus allowing a direct comparison between both installed systems.

Illustration 8 shows the average values for selected gas substances of the year 2005.

The comparison shows that the Conditioning Rotor – Recycle Process with particle conditioning is equal to the more complex wet system. The only difference is the reference variable for the separation of the acid crude gas components, i.e.  $\text{SO}_2$  for the scrubber and  $\text{HCl}$  for the conditioned dry sorption.

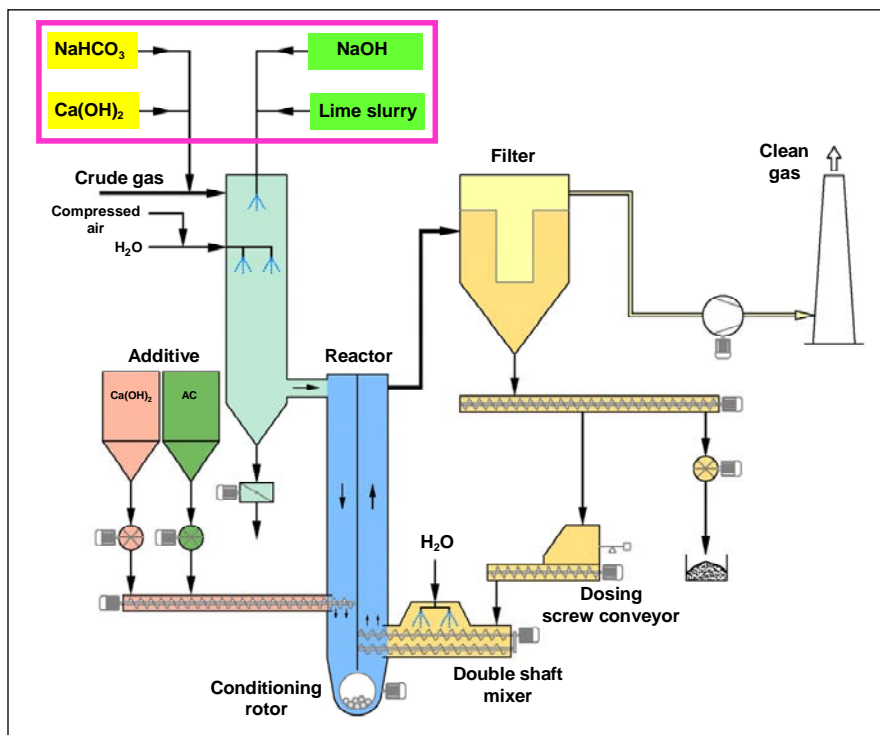


III. 8: Comparison of gas cleaning systems „wet“ and „conditioned dry“ (2005)

### 3 Conditioning Rotor – Recycle Process with graded additive powder injection

As a result of the ban on landfill of higher caloric substances in Germany in the year 2005, incinerators for RDF (Refuse Derived Fuel) have been installed for many applications beside the conventional waste incinerators. Compared to the untreated waste, the used fuels are often containing definitely higher Cl- and S-concentrations. The crude gas values measured at realised plants downstream boiler, often total to  $> 2500 \text{ mg/Nm}^3$  for HCl and  $> 1500 \text{ mg/Nm}^3$  for  $\text{SO}_2$  in continuous operation.

With regard to these high crude gas values and when using the technology described in section 2 of this lecture without any additional measures, the stoichiometry has to be increased partly definitely above a typical base value of 2 in order to observe reliably the emission limit values. Regarding these types of applications it will be advisable to use a graded additive powder injection, thus using in addition the reaction chamber of evaporative cooler when indicated. Illustration 9 shows different, corresponding process variants. For all concepts, the main quantity of additive powder is in the nominal case injected into the reactor downstream evaporative cooler. The injection of additive powder upstream or inside of evaporative cooler mainly serves for the corrosion protection as well as for the smoothening of crude gas peaks.

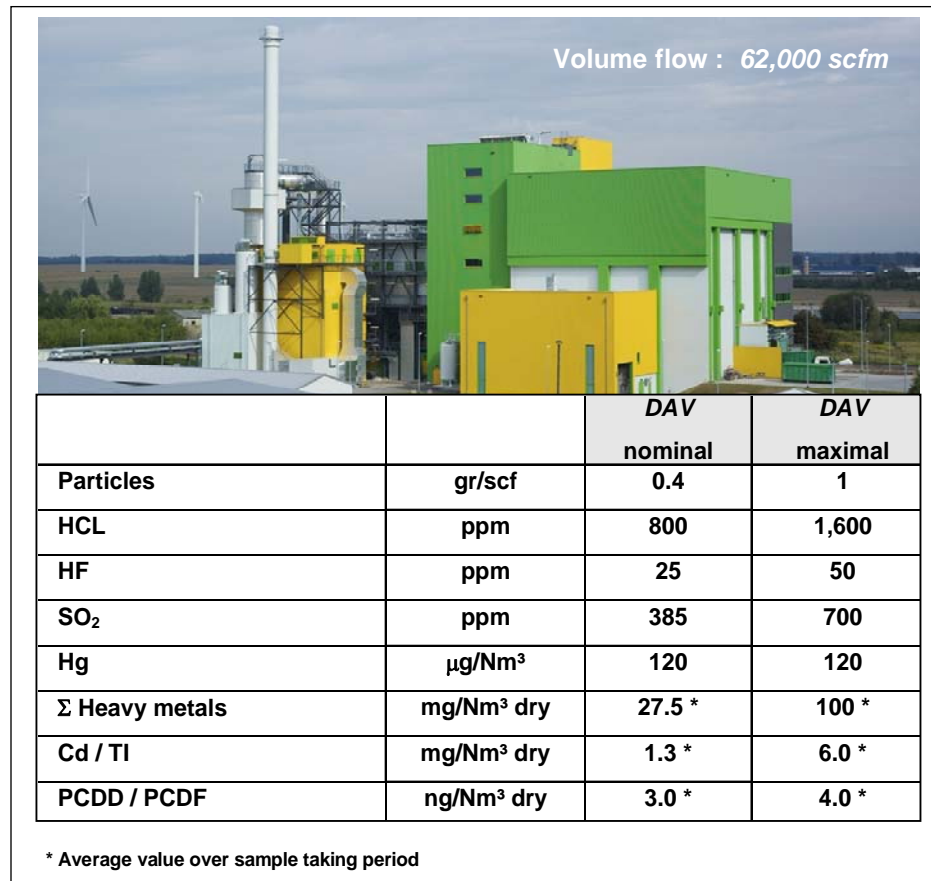


III. 9: Conditioning Rotor – Recycle Process with graded additive powder injection

All process variants have already been realised. The preferred system is the graded injection of  $\text{Ca(OH)}_2$  upstream and downstream of evaporative cooler, among other things due to the very economic feasibility.

### 3.1 Application example

Illustration 10 shows the RDF incineration at Stavenhagen/ Germany as representative for several realised plants, executed as Conditioning Rotor – Recycle Process with graded additive powder injection. The table in this illustration specifies the gas substances downstream boiler relevant for the gas cleaning.



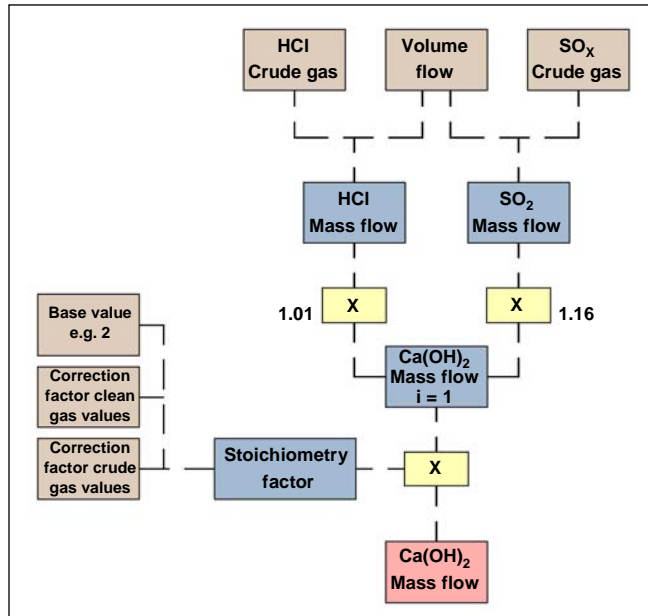
Il. 10: RDF incineration plant Stavenhagen / Germany

Especially noticeable is the max. daily average value for SO<sub>2</sub>, totalling to up to 700 ppm. Half-hour average values or peaks can, of course, be definitely higher. The requested emission limit values according to EU directive can reliably be kept in continuous operation.

- Acid crude gas components

The injection quantity of Ca(OH)<sub>2</sub> is controlled subject to a given stoichiometric factor (ill. 11). The necessary additive powder mass flow is calculated according to the adjusted stoichiometric factor and on the basis of the volume flow and the HCl and SO<sub>2</sub> values, which are continuously measured in the crude gas upstream evaporative cooler. In addition to this and in case of increased crude gas values, the stoichiometric factor is automatically increased by means of a superposed adjustment curve.

Furthermore, the monitoring of the emission values, combined with the increase in the injection quantity in case of reaching the clean gas limit values for HCl and SO<sub>2</sub>, ensures that the emission values (DAV and HAV) will by no means be exceeded.



III. 11: Control scheme Ca(OH)<sub>2</sub> injection

The graded additive powder injection allows to achieve and/or to undercut the intended stoichiometric factor of 2 with reliable observance of emission limit values. The averaged stoichiometric factor actually reached in continuous operation has repeatedly been determined by means of remainder analyses. It lies in a range between 1.8 up to 2.0. Table 3 exemplary shows the corresponding analysis of a material sample taken in October 2007. The stoichiometric factor is in this case < 1.9. The Cl content totals to approx. 20 weight%, thus lying in a range, noncritical for the product handling.

Analysis	Value [%]	Ca content in substance	Ca(OH) <sub>2</sub> content in substance	Residual lime, calculated as Ca(OH) <sub>2</sub>
Σ Ca	29.8			
CaSO <sub>3</sub>	5.25	1.8	3.2	
CaSO <sub>4</sub>	7.92	2.3	4.2	
CaCO <sub>3</sub>	8.07	3.2		6.0
CaCl <sub>2</sub>	31.4	11.4	21.1	
CaF <sub>2</sub>	0.23	0.1	0.2	
Ca(OH) <sub>2</sub>	18.0	9.7		18.0
Sum			28.7	24.0

Ca(OH)<sub>2</sub> input : 28.7 + 24.0 = 52.7  
 converted Ca(OH)<sub>2</sub> : 28.7  
 Stoichiometry i : i = 52.7 ÷ 28.7 = **1.83**

Tab. 3: Calculation of stoichiometry based on remainder analysis

- Dioxins/ Furans and Hg as well as Hg compounds

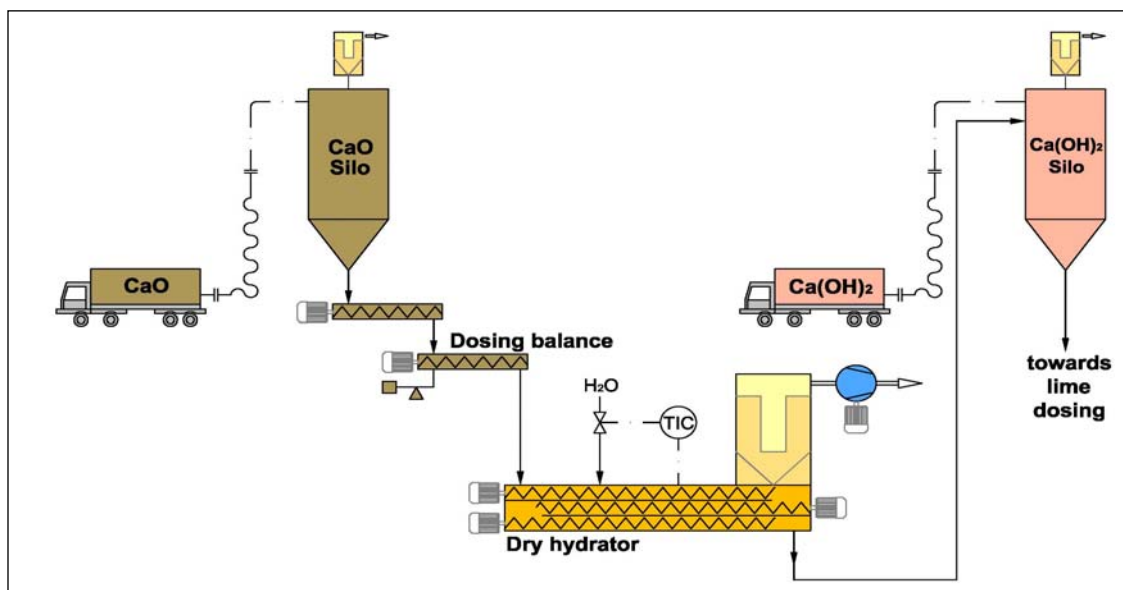
Activated carbon with a standard dosing quantity is used as additive powder for the separation of mercury and/or mercury compounds and dioxins/furans. The continuously measured Hg clean gas values are definitely  $< 5 \mu\text{g}/\text{Nm}^3$  dry. Measuring results for PCPP/-F are listed in table 4.

	n	Maximum [mg/m <sup>3</sup> ]	Extended measuring uncertainty	Limit value	Condition of highest emission
PCCD/PCDF	1	0.0015 ng/m <sup>3</sup>	0.0002 ng/m <sup>3</sup>	0.1 ng/m <sup>3</sup>	yes
Benzopyrene	3	$< 0.0022$	0.0002	0.009	yes

Tab. 4: Results of dioxin/furan measurements at WtE plant Stavenhagen

#### 4 Utilisation of CaO instead of Ca(OH)<sub>2</sub> for the reduction of operating costs

In case of the conditioned dry sorption, the Ca-based additive powder is injected into the reactor dry in form of Ca(OH)<sub>2</sub>. Compared to the use of CaO as e.g. for the spray sorption, this presents a disadvantage due to the higher purchase costs for Ca(OH)<sub>2</sub>. In order to compensate this cost disadvantage, plants with a higher additive powder consumption are often provided in addition with a dry hydrator for CaO. In this case, the additive powder is supplied in form of CaO. It is converted to Ca(OH)<sub>2</sub> by means of H<sub>2</sub>O injection in a dry hydrator and is stored in an intermediate silo for the injection into the reactor and/or also upstream evaporative cooler as dry additive powder. The intermediate silo is adequately dimensioned to allow a direct filling of silo with Ca(OH)<sub>2</sub> in case of maintenance and repair works near the dry hydrator. A corresponding scheme is shown in illustration 12.



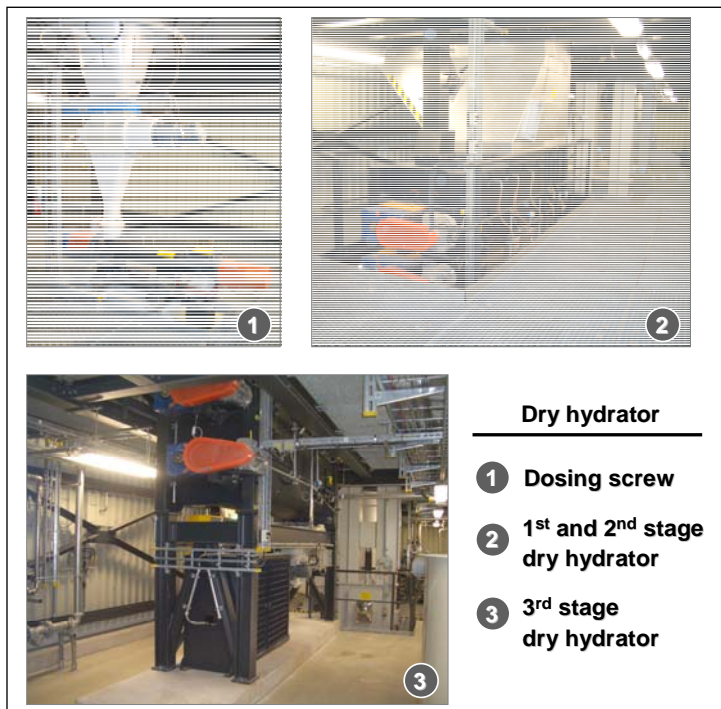
III. 12: Rough scheme dry hydration CaO

Several plants in Germany have been provided with this technology. Illustration 13 shows a plant, realised with a dry hydrator for a  $\text{Ca(OH)}_2$  production capacity of approx. 3.5 tn/h (ill. 14).



Ill. 13: RDF incineration plant EEW Premnitz/ Germany

As alternative there is the possibility to install the dry hydrator close to the additive powder injection point near the reactor. The produced  $\text{Ca(OH)}_2$  can now be injected directly into the reactor without temporary storage in a silo. This variant will not be possible in case of a graded additive powder injection.



Ill. 14: Dry hydrator for  $\text{CaO}$

## 5 Advantages of conditioned dry sorption compared to the spray sorption

Comparative examinations regarding the additive powder utilisation have been realised at a plant in Germany, provided with both a spray sorption and a conditioned dry sorption. The result was a definitely lower additive powder consumption in case of consistent operation of dry sorption compared to the spray sorption. The relevant reasons for this are:

- Formation of  $\text{CaCO}_3$  during the aqueous phase

Compared to the acid crude gases  $\text{HCl}$ ,  $\text{HF}$  and  $\text{SO}_2$ , the slightly acid carbon dioxide has a minor affinity to hydrated lime. However, the concentration of  $\text{CO}_2$  within the gas is definitely higher. A  $\text{CO}_2$  concentration of approx. 10%Vol., corresponding to 100,000 ppm, is faced with a  $\text{HCl}$  concentration of e.g. 1,600  $\text{mg/m}^3$ , corresponding to 1,000 ppm. During the wet phase a considerable amount of  $\text{CaCO}_3$  will be formed which – after drying of lime slurry drops – will be only very limited available for the reaction.

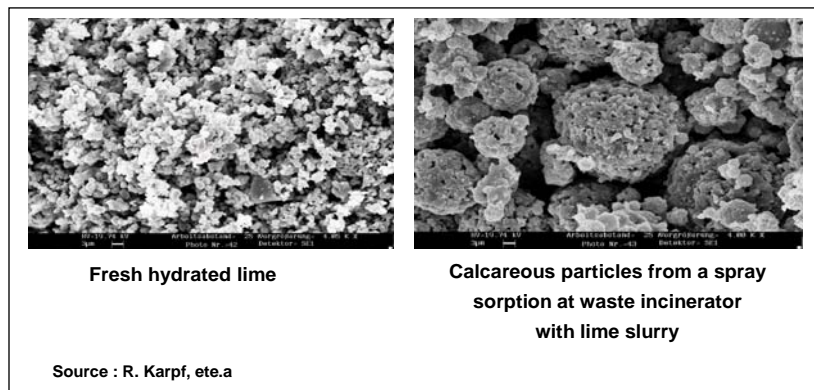
A disadvantage of incinerators for waste and alternative fuels is, that due to the hygroscopic features of  $\text{CaCl}_2$ , a temperature reduction to values definitely below  $140^\circ\text{C}$  and by this a possible reactivation of the  $\text{CaCO}_3$  during the wet phase will not be possible. In case of a corresponding water injection, the downstream installed conditioned dry sorption may lead to a partial reactivation of the  $\text{CaCO}_3$ .

- Formation of agglomerates

The microscopic photos in picture 15 show fresh hydrated lime particles compared to calcareous particles extracted downstream spray absorber. The freshly slaked hydrated lime has a clearly visible, high outer surface. However, after drying within spray absorber, this will be reduced due to the formation of drop shaped agglomerates. The exchange surface necessary for the chemical reaction will be reduced.

- Influence of particle re-circulation

As described in section 2 of this lecture, the multiple particle re-circulation of the conditioned dry sorption creates a higher particle density within reactor and increases the residence time of additive powder. In addition, the separation conditions within filter will be improved.



III. 15: Surface structure of  $\text{Ca}(\text{OH})_2$ , upstream and downstream spray absorber

- Due to the multiple particle re-circulation, the conditioned dry sorption offers advantages regarding the separation of dioxins/ furans and mercury. Last but not least, even in case of crude gas peaks, the limit values will reliably be observed with low AC injection.

## 6 Assessment

The present operating experiences gathered from a multitude of realised plants with Conditioning Rotor – Recycle Process with particle conditioning confirmed its potential and reliability.

- The requested emission limit values are reliably kept in continuous operation
- Crude gas peaks are reliably compensated due to the large additive powder potential within the plant
- The stoichiometric factor for the  $\text{Ca}(\text{OH})_2$  injection for the separation of acid crude gas components normally totals to a value of approx. 2
- CaO can be used as additive powder with saving of costs
- The injection quantity for AC totals to a specific value of approx. 0.03 gr/ scf
- The comparatively simple structure grants a high availability
- Higher requirements on the separation of acid crude gas e.g. due to high crude gas values, can be compensated in a simple way by means of the graded additive powder injection



Enzer Str. 26  
31655 Stadthagen  
GERMANY

phone: +49 (0) 5721 708 - 200  
fax: +49 (0) 5721 708 - 154  
e-mail: [info@luehr-filter.de](mailto:info@luehr-filter.de)

Internet: [www.luehr-filter.de](http://www.luehr-filter.de)